











A Novel Formulation of LV Distribution Network Equivalents for Reliability Analysis

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Single-Line (1-ph) vs Three-Phase (3-ph) Models

Three-phase model of an 'unbalanced' (& realistic) generic suburban LV network





Single-line model of a 'balanced' generic suburban LV network

Ignores phase-connection of customers, and protection system components (single-pole vs three-pole)

Reliability Performance of MV networks



Volume and complexity!

Use lumped aggregate model for each LV network with total load & number of customers

Reduce computation times for reliability assessment

Inaccurate representations

- Neglect the highly dispersed loads and
- different component types

- Large cumulative errors
- Incorrect characterisation of the quality of supply for different customers
- Affects network planning and operation

State Enumeration

- State Enumeration (SE) is used to perform reliability analyses of large networks.
- Usually, for a system of m repairable components, there are 2^m system states.
- Each state is a combination of the status of different components (UP/DOWN).
- It is **not computationally feasible** to enumerate all system states for large systems.
- Usually, the **analysis stops** at a given enumeration depth (ED), which corresponds to a failure level.

$$ED_k = C_0^m + C_1^m + \dots + C_k^m$$
For a system of $k = 97$ components:System states with: $ED_1 = C_0^m + C_1^m$ $ED1 = C_0^{97} + C_1^{97} = 98$ statesOnly 1 component failure $ED_2 = C_0^m + C_1^m + C_2^m$ $ED2 = C_0^{97} + C_1^{97} + C_2^{97} = 4754$ statesOnly 2 component failures

State Enumeration cont'd

- The **frequency of occurrence** of each system state and the **mean duration** of residing in each state is based on the **failure and repair rates of components**.
- The impact of each selected state must be identified in terms of the interrupted loads/customers.
- Sequential **Monte Carlo Simulation (MCS)** can then be used to calculate reliability indices based on an artificial cycle of system operating and failure states.

Considering only low-order contingencies

- Reduced computational efforts without significantly impacting accuracy
- Successive transitions between two system failure states are very rare.

Considering only high-order contingencies

- System resilience
- Protection design & control

Sequential Monte Carlo Simulation

- Sequential MCSs are usually performed using state duration sampling (SDS)
- Each component is assigned a mean failure rate and mean repair time
- Creating a state transition process of the up and down cycles of all system components.

BUT

- The SE-reduced number of states (r) do not distinctly equate to an equivalent number of components.
- For example, $r = C_0^{97} + C_1^{97} = 98$ states for ED_1 of the Single line model.
- This corresponds to a fictitious number of components between 6 $(2^6 = 64)$ and 7 $(2^7 = 128)$.
- SO, we use sequential MCS based on state transition sampling (STS)
- STS focuses on state transitions of the entire system, rather than on the individual component states
- The system will transit from one system state S_k into the next state S_{k+1} depending on the random state duration of the component that first departs from its present state (up or down) in system state S_k

Sequential MCS cont'd

The probability of the j^{th} component departing from present state at time t_0 is:

 $P_j = \frac{\lambda_j}{\sum_{i=1}^m \lambda_i}$

The state transition of any component leads to a state transition. For m components, there can be m possible reached states.

The probability of the *m* states that could be reached can then be successively placed in the interval [0,1] (because $\sum_{j}^{m} P_{j} = 1$)

Assess the consequences of each system state, i.e., the impact on frequency and duration of customer interruptions.

Simulation is repeated until the required accuracy ε

i = 1, 2, ..., m, where m is the number of components



Generate a uniformly distributed random number R_i between 0 and 1.

$$\varepsilon = \sqrt{var(x)}/(\bar{x}\cdot\sqrt{N})$$

Formulation of Reliability Equivalents of LV Networks



- Formulate Unavailability (U), using Energy Not Supplied (ENS).
- ENS combines both frequency- and duration-based indices.
- It is a **composite reliability performance indicator** that quantifies the combined effects of the numbers and durations of supply interruptions with the amount of interrupted demand.

$$\lambda_{eqv} = SAIFI \times LPs$$
 $U = \frac{Annual ENS}{Connected demand \times hours in a year}$

$$U = \frac{\lambda_{eqv}}{\lambda_{eqv} + \mu_{eqv}} \qquad \qquad \mu_{eqv} = \frac{(1-U)\cdot\lambda_{eqv}}{U} \qquad \qquad MTTR_{eqv} = \frac{1}{\mu_{eqv}}$$

State Enumeration and Monte Carlo Simulation Techniques



Single-Line (1-ph) vs Three-Phase (3-ph) Models



- TPM is **more accurate**;
- Detailed representation of the actual network;
- SLM **underestimates** reliability performance, mainly for ENS;
- TPM differentiates different fault types.
- Low-order EDs are sufficient to assess reliability performance with high accuracy, while requiring significantly shorter computational times.

Combining SE and SMCS for LV Reliability Equivalents

- ED_1 and ED_2 produce **nearly identical** results due to the low probability of double faults.
- ED_2 results in much longer simulation times than for ED_1
- Computational time is reduced by 99.9% for ED_1 and by 91.1% for ED_2 models compared to original network.
- The time required to perform equivalenting is also higher in ED_2 (33.8 hours) than ED_1 (2.5 hours)
- ED_1 is sufficiently representative of the original network.

Network	SAIDI		SAIFI		ENS	
	hrs/c/y	Error	ints/c/y	Error	kWh/c/y	Error
Orig.	0.9508	-	0.0588	-	5.7648	-
ED ₁	0.9739	2.4%	0.0576	2.0%	5.8437	1.4%
Eqv-PC	0.9154	3.7%	0.0577	1.9%	5.8485	1.5%

Reliability Indices for the TPM Equivalent Component.

Combining SE and SMCS for LV Reliability Equivalents



11/15



- Combined SE–SMCS (ED₁) \equiv Original network
- Eqv-PC aggregates composite reliability information
- Still adequately approximates the CDFs of the detailed original network with a higher number of components.
- Quantifying the risk of longer interruption times, frequency and ENS.

Analysis at MV Level with LV Network Equivalents



Eqv-PC	λ _{eqv} (failures/year)	MTTR _{eqv} (hours)
SE-SMCS	1.052	1.217
AEM	0.472	6.235

SE-SMCS approach:

- Location of components;
- Impact of failures;
- <u>Does not</u> increase complexity;
- Reliability dependency between MV and LV networks.



Conclusions

- A novel comparison of the (typically used) simplified SLMs of LV networks, in contrast with fully detailed TPMs, which **avoids systems' performance overestimation**.
- Development of a novel LV/MV network reliability assessment methodology that **combines SE and SMCS** to significantly reduce computational complexity while preserving accuracy.
- Development of a novel and simple **single-component network equivalent**, which offers the same **unavailability** (and therefore reliability performance) as the original LV/MV network.
- Accuracy, computational efficiency and scalability of the proposed LV equivalents is tested and validated in more complex and larger MV networks, for **replicability** of the proposed methodology.

Thanks for listening. Any Questions?

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