

How Fragility Modelling Assumptions Influence Power System Resilience Assessments

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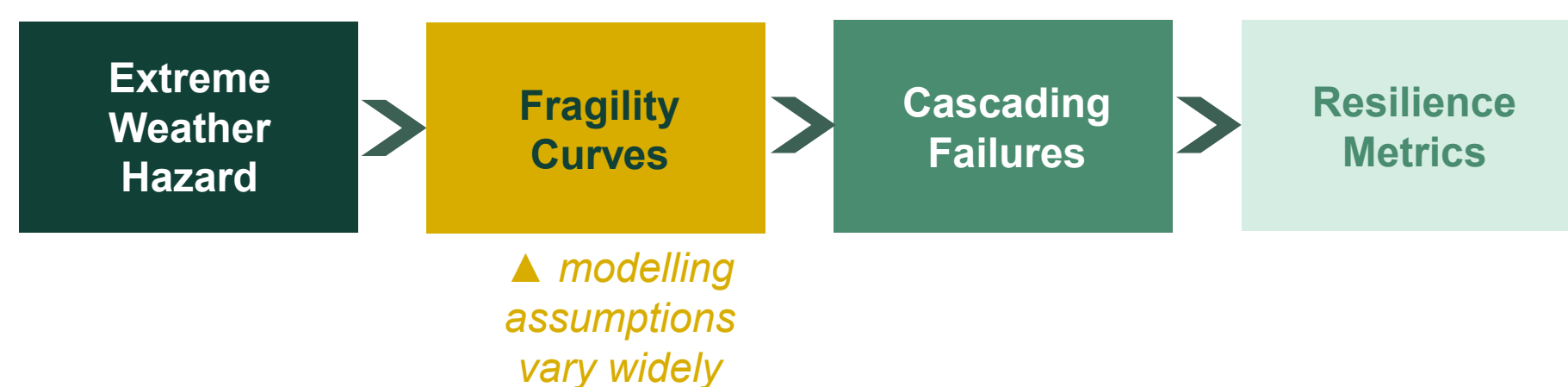
Background & Research Gap

~1 Million

customers without power for up to 7 days

Storm Arwen¹ 2021 UK

Extreme weather increasingly threatens transmission networks. Fragility curves quantify component failure probability vs. hazard intensity, but modelling assumptions vary widely, and those choices can significantly alter system-level resilience estimates.



Research Question:

How do fragility curve assumptions shape grid resilience estimates?



Power System Resilience

The ability to limit the extent, severity and duration of system degradation following an extreme event.

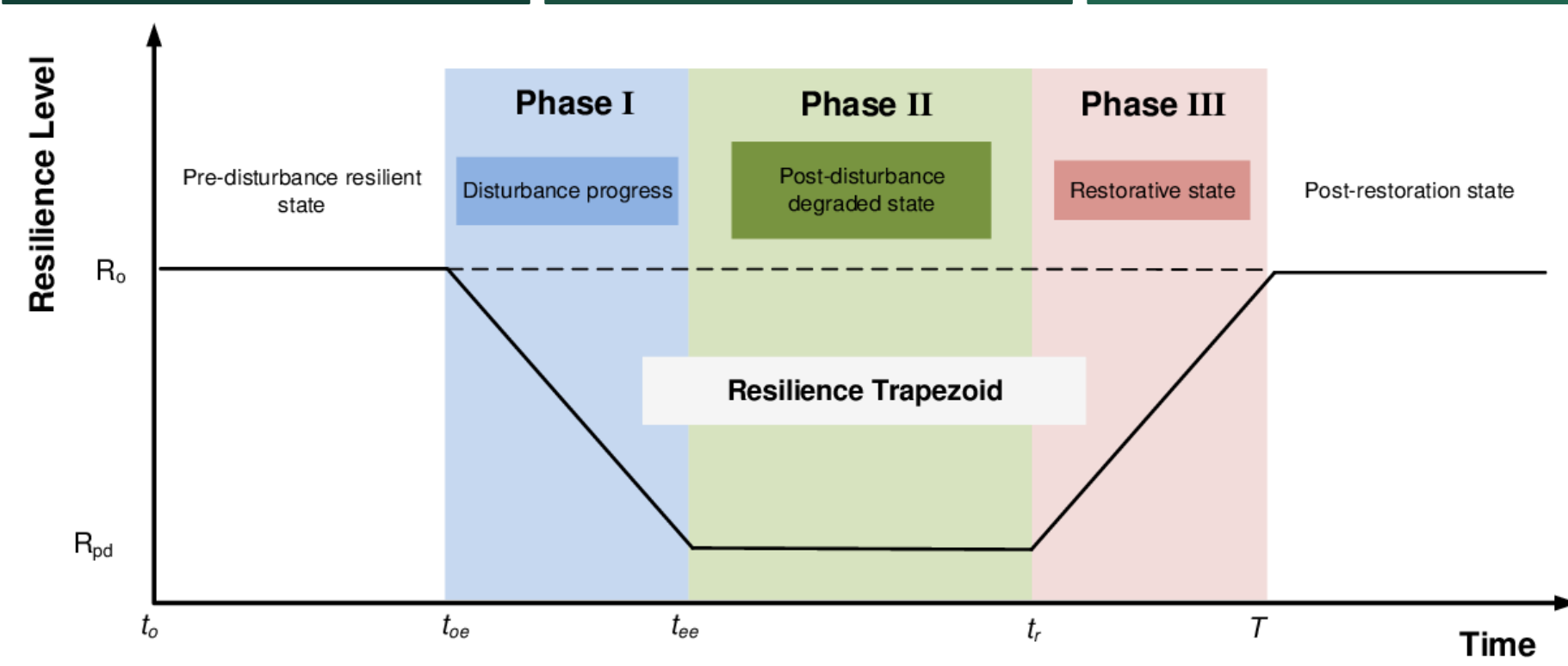


Fig. 1: Resilience trapezoid: three phases from event onset to restoration²

Assumption A: Asset Health

Ofgem's CNAIM/NARM health scores H derived from age, corrosion and loading.

$$H(t) = H_{new} \cdot e^{\beta \cdot t} \cdot F_{cond} \cdot F_{rel}$$

Asset health index

$$PoF = K \left(1 + CH + \frac{(CH)^2}{2!} + \frac{(CH)^3}{3!} \right)$$

Failure probability, shifts curve left as H increases

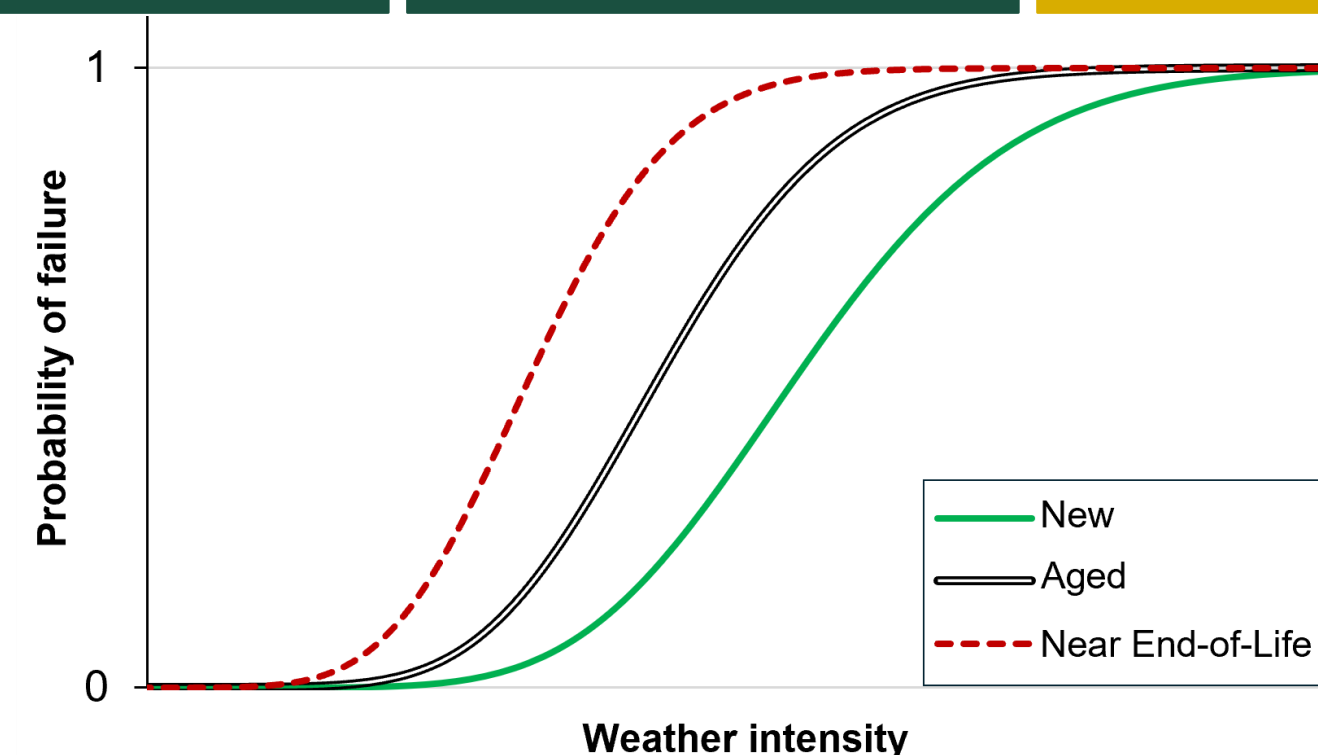
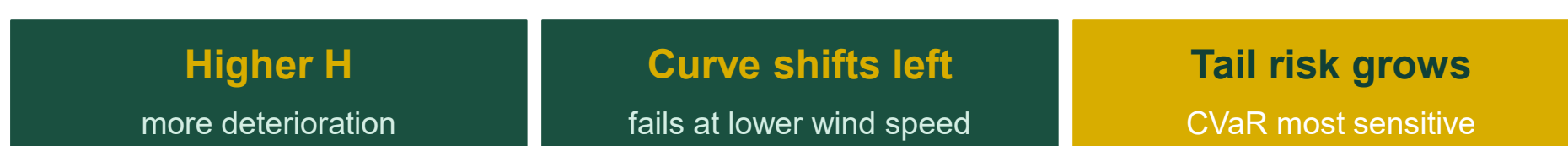
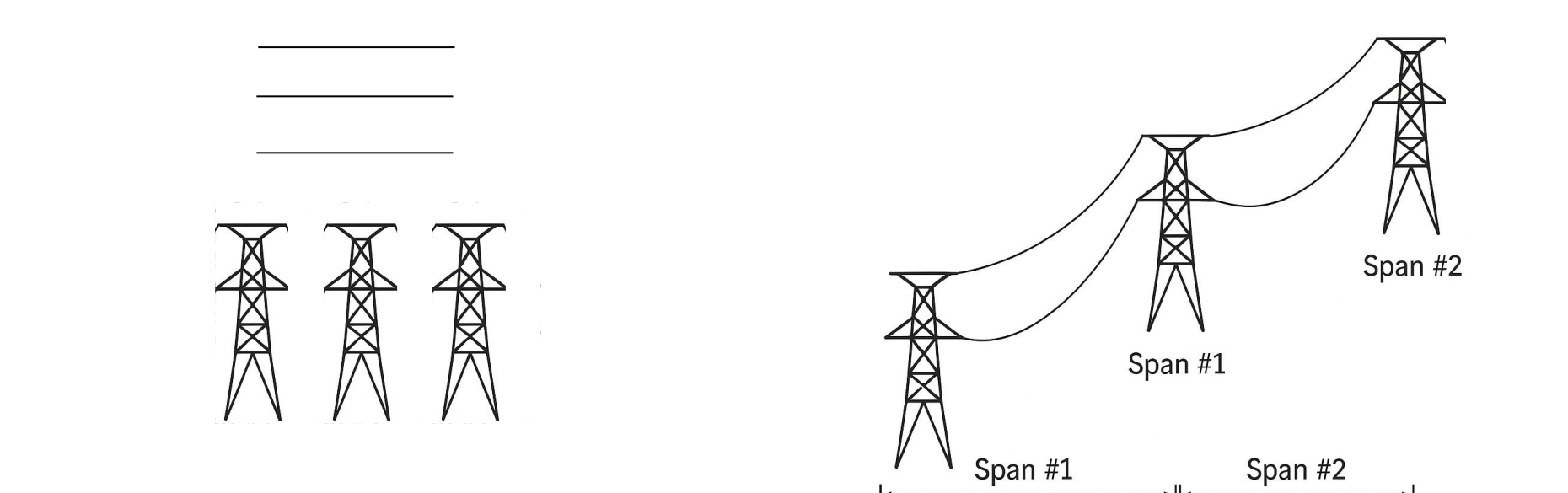
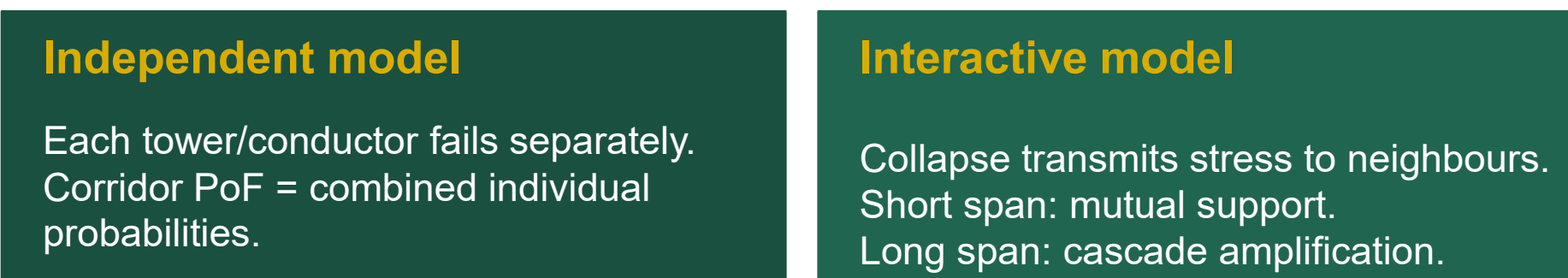


Fig. 2: Fragility curves shift left as asset health deteriorates

Assumption B: Tower-Line Interactions

Tower collapse transmits mechanical tension to adjacent towers via conductor. A 3-tower 2-line prototype captures this coupling.



Short exposure: Mutual support → Interactive < Independent PoF
Long exposure: Cascade amplification → Interactive > Independent PoF

Assumption C: Spatio-Temporal Dynamics

Storm epicentre moves hourly. Attack angle θ and distance continuously update each component's fragility parameters.

$\theta = 90^\circ$ (perpendicular wind) → maximum structural stress on towers

$$\mu = \mu_{base} - \frac{P_{norm}(H)}{5} + \frac{\cos(\theta)}{5}$$

Location param, shifts left with health deterioration and favourable angle

$$\sigma = \sigma_{base} - \frac{P_{norm}(H)}{10} + \frac{\cos(\theta)}{50}$$

Scale param, narrows (steeper curve) as health worsens

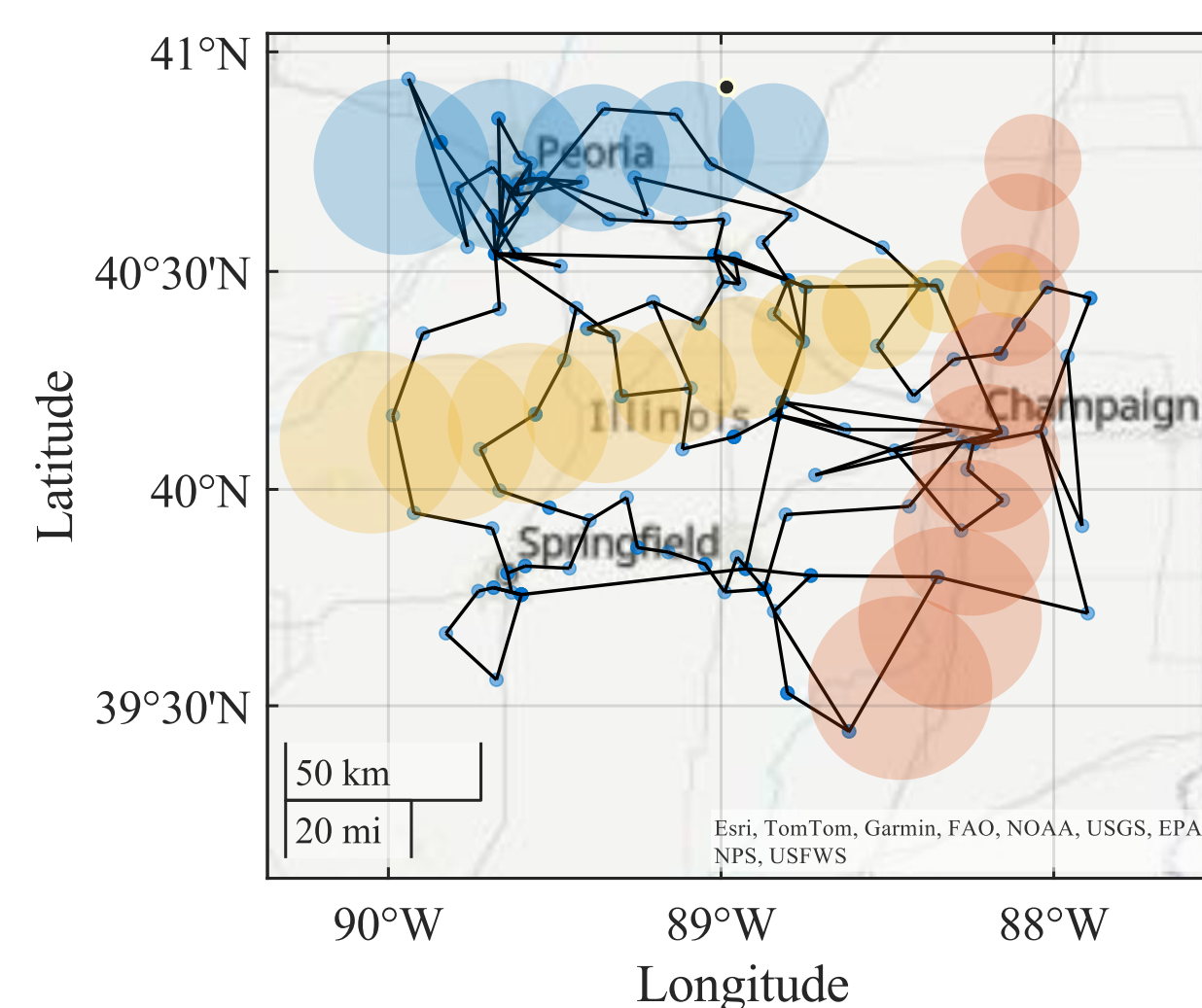
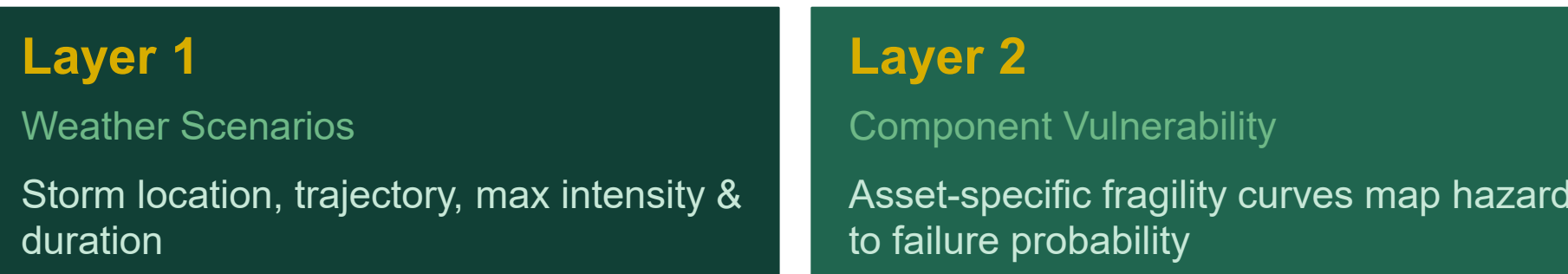


Fig. 3: Three storm trajectories over ACTIVSg200 Illinois network; circles = hourly epicentres

Sequential Monte Carlo Framework



Per-scenario simulation loop:

- 1 Identify: Exposed components in storm impact zone per hour
- 2 Map: Apply fragility curves → determine component failures
- 3 Cascade: DC power flow → overload detection → removal → repeat until stable
- 4 Advance: Record system state; use as t+1 initial condition
- 5 Repeat: Until event duration elapsed
- 6 Quantify: Compute EDNS, VaR₉₅, CVaR₉₅ across full ensemble

Cascading failure model

Quasi-static DC OPF · iterative overload detection & component removal · load shedding & generator tripping · convergence: $\Delta EDNS < 10^{-6}$

Study Cases: ACTIVSg200 Illinois

200 Buses	179 Lines	1.48 GW Peak Demand
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Windstorm max speed: 30–60 m/s (hurricane-force)
Random entry location & trajectory

Four modelling scenarios:

Case 1 BASELINE All three assumptions active (A + B + C)	Health ✓	T-L ✓	Spatio-T ✓
Case 2 -A Uniform health H=2, no asset health variability	Health X	T-L ✓	Spatio-T ✓
Case 3 -B Independent T/L failures, no tower-line coupling	Health ✓	T-L X	Spatio-T ✓
Case 4 -C Uniform wind, no spatio-temporal dynamics	Health ✓	T-L ✓	Spatio-T X

Resilience Metrics

EDNS Expected Demand Not Served Mean DNS across all Monte Carlo trials (MW)	VaR₉₅ Value-at-Risk (95th pct.) Worst-case DNS level not exceeded in 95% of runs	CVaR₉₅ Conditional VaR (95th pct.) Mean DNS in the extreme 5% tail, captures rare catastrophic events
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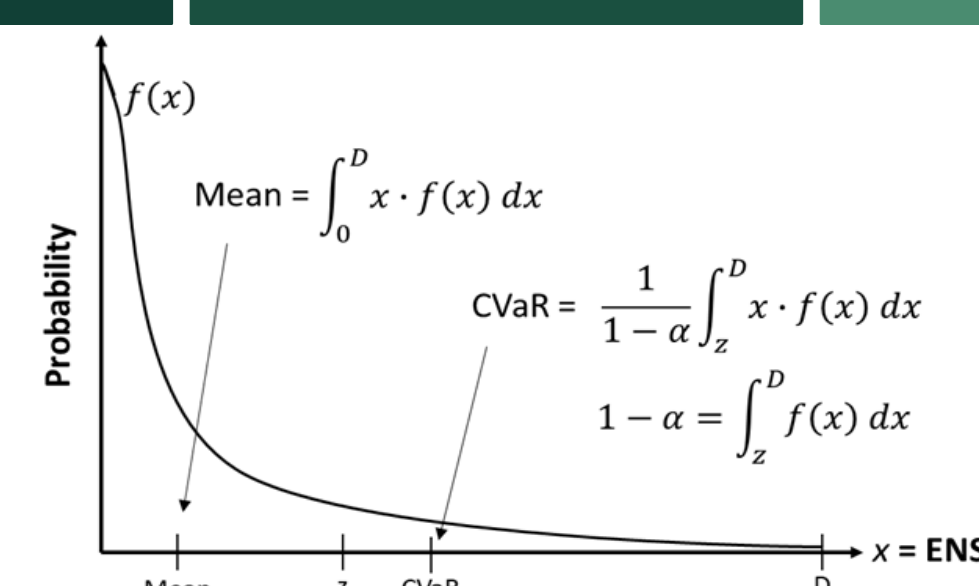


Fig. 4: Statistical risk metrics derived from the Monte Carlo DNS ensemble

Results: Tower-Line Interaction Effect

Crossover ~5 km: interactive < independent PoF (mutual tower support)

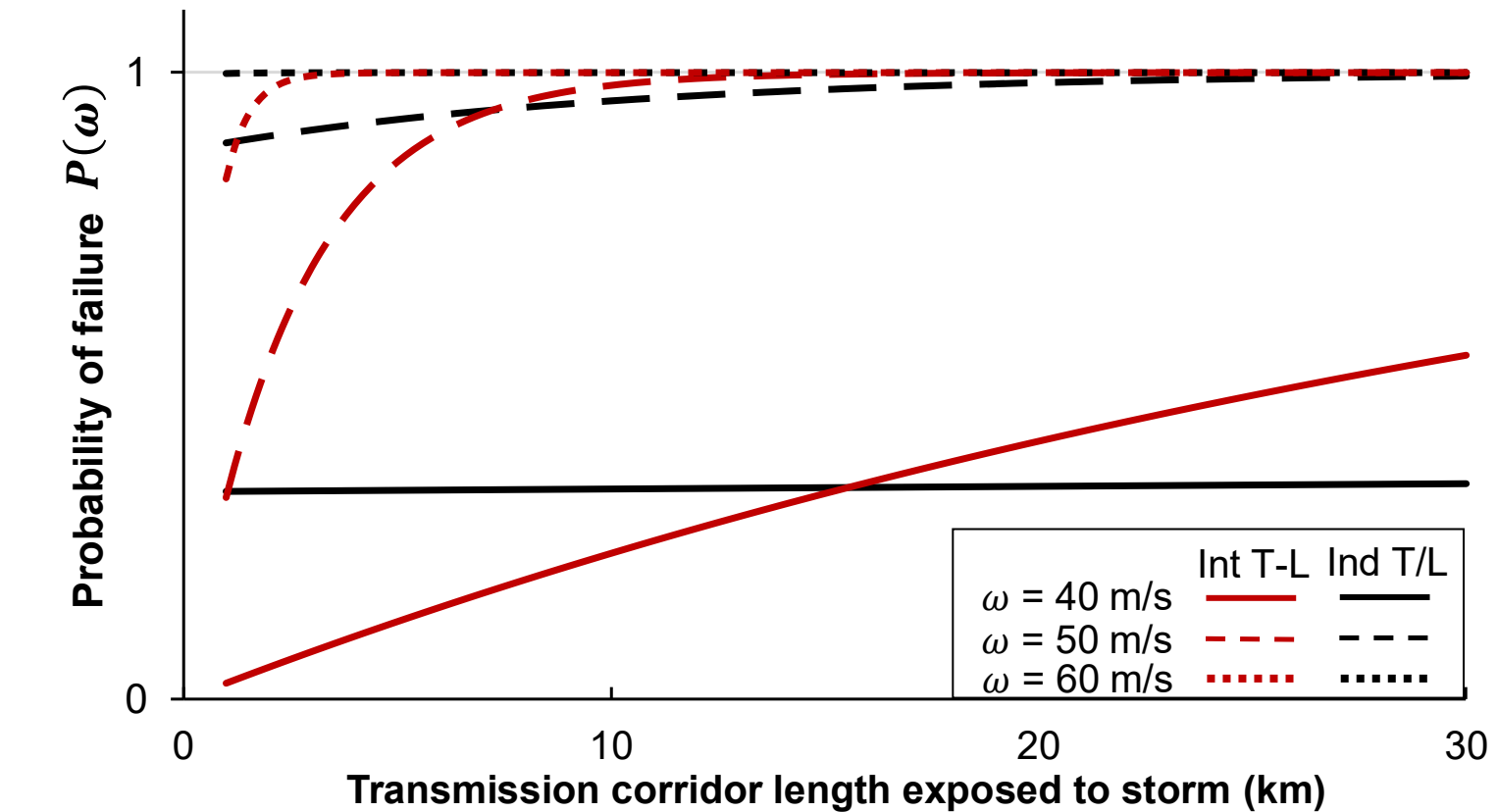


Fig. 5 Corridor failure probability vs. storm-exposed length: interactive vs. independent

Results: Demand-Loss Distribution (Health)

Case 1 (Variable H) >1300 MW max loss Fewer loss events (15% exceed 10 MW) but higher severity, tail risk driven by aged assets.	Case 2 (Uniform H=2) 723 MW max loss More frequent but milder losses (37% exceed 10 MW). Masks catastrophic tail risk.
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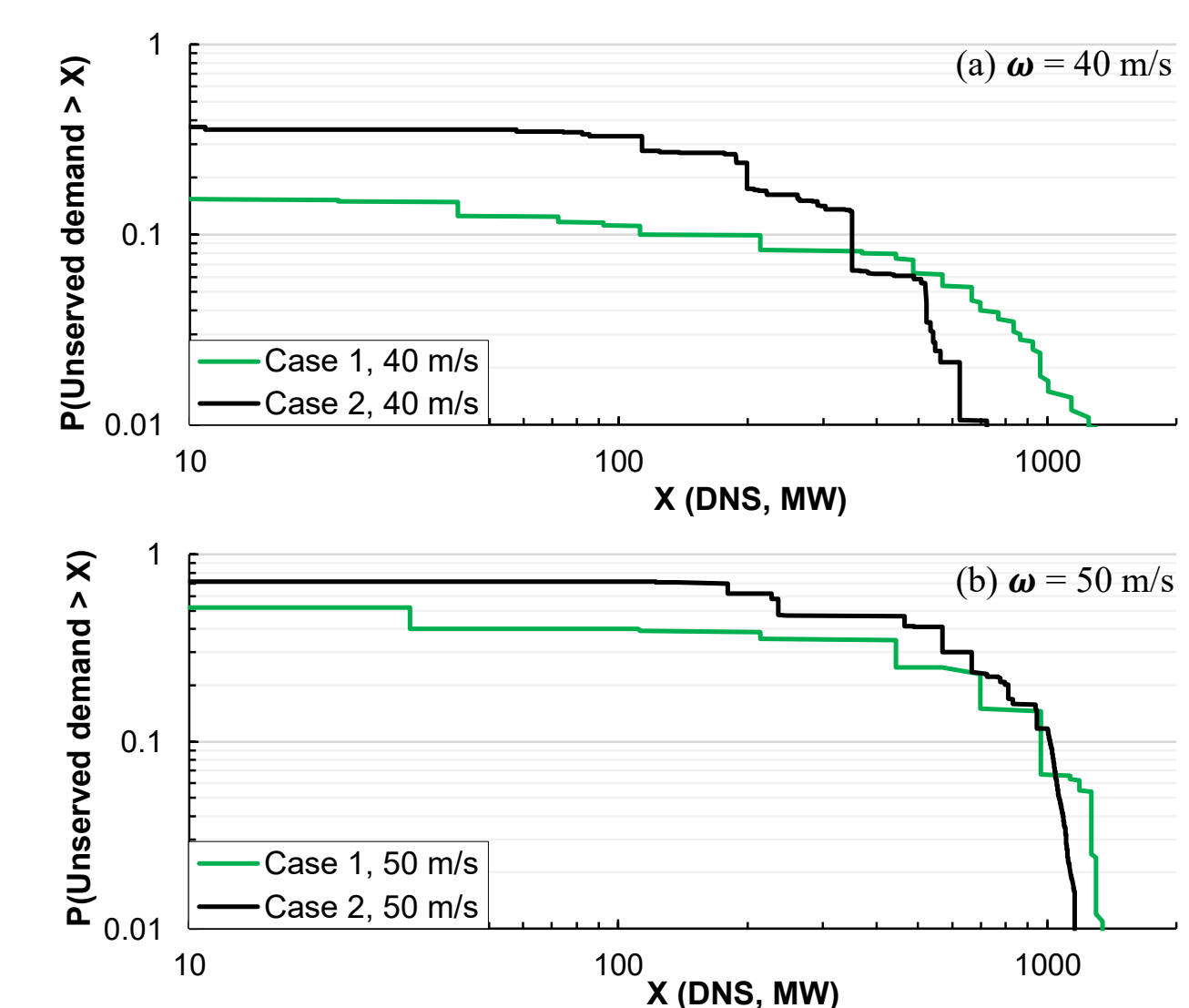


Fig. 6: Complementary CDF of DNS: Case 1 vs. Case 2 at 40 m/s and 50 m/s

Results: Quantitative Comparison

EDNS, VaR₉₅ and CVaR₉₅ (MW), Case 1 vs Case 2, fixed trajectory storm

Metric	Case	40 m/s	50 m/s	60 m/s
EDNS (MW)	Case 1	121.6	442.8	1051.4
	Case 2	83.2	328.0	986.1
VaR ₉₅ (MW)	Case 1	656.3	1265.1	1272.8
	Case 2	518.6	1065.5	1272.8
CVaR ₉₅ (MW)	Case 1	986.0	1278.1	1290.8
	Case 2	596.5	1130.0	1290.8

- 32% EDNS underestimate at 40 m/s, peaks at moderate intensity
- < 1% Converges at 60 m/s, catastrophic saturation masks differences

Conclusions

- 1 Asset health is the most critical assumption
-18% EDNS when health variability omitted
Omitting health variability produces systematically optimistic estimates, especially at moderate intensities. CNAIM scores provide a practical, data-ready basis.
 - 2 Tower-line structural coupling must be included
+17% EDNS when coupling excluded
Independent assumptions both under- and over-predict risk depending on corridor length. Interaction provides mutual support at typical ~5 km spans.
 - 3 Spatio-temporal dynamics: scenario-critical, ensemble-stable
-2% EDNS difference over large ensembles
Attack angle and trajectory drive large variation in individual scenarios but average out across the ensemble. Critical for worst-case planning, not mean-risk.
 - 4 Modelling complexity should match the application context
Moderate Intensity, highest sensitivity
Tailored fragility models add most value at moderate events. Under catastrophic extremes, systemic network vulnerability dominates and simpler models carry reduced penalty.
- Key Insight: Tailored fragility modelling is most valuable at moderate hazard intensities. Under extreme events, network topology and systemic overload dominate all individual modelling assumptions.

Acknowledgement

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References

1. Ofgem, "Final report on the review into the networks' response to Storm Arwen," 2022.
2. IEEE Task Force on Methods for Analysis and Quantification of Power System Resilience, "The Definition and Quantification of Resilience," Tech. Rep. IEEE PES-TR65, 2018.